



Unexpected role of singlet oxygen generated in urea-modulated LaFeO₃ perovskite heterogeneous Fenton system in denitrification: Mechanism and theoretical calculations

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ABSTRACT

This study appears an unprecedented phenomenon that ¹O₂, generated in urea-modulated LaFeO₃ (U-LaFeO₃) perovskite heterogeneous Fenton system, is superior to OH• and O₂•⁻ in NO removal. The 2.5 U-LaFeO₃/H₂O₂ system can remove 82.99% of NO, with a low H₂O₂/NO molar ratio (4.7) and high GHSV (30,800 h⁻¹), along with good environmental adaptability and reusability. Urea modulation induced the formations of abundant La defects, O vacancies and Fe(IV), also improved the pore structure and surface area. The contribution order of different free radicals to NO removal is ¹O₂ > xO₂•⁻ > •OH. Characterization combined with theoretical calculation clarify that (i) H₂O₂ is inclined to derive HO₂• on Fe sites; (ii) ¹O₂ is mainly generated from O₂•⁻ reaction with Fe(IV)/Fe(III); (iii) •OH is mainly produced by splitting of H₂O₂ on Fe site and decomposition of HO₂• on OV site. The main denitrification paths are NO + ¹O₂ → NO₂, NO₂ + •OH → NO₃ and NO + •OH → NO₂.

1. Introduction

As a primary atmospheric pollutant, nitrogen oxides (NO_x, composed of ~95% NO) are the main precursors for ozone, photochemical smog, haze and other environmental issues, posing enormous threats to human health [1,2]. To reduce NO_x emissions from stationary source, the mature selective catalytic reduction (SCR) and selective non-catalytic reduction (SNCR) technologies have been widely applied, but they still cannot be adaptive for all working conditions due to narrow applicable temperature ranges [2–5]. In some cases, the SCR or SNCR alone is very difficult to meet ultra-low emission standard of NO_x (≤50 mg/m³). Hence, developing low temperature denitrification method that can couple with the SCR or SNCR system to realize deep removal of NO_x is urgently needed. In this respect, advanced oxidation process (AOP) is a good supplement [6,7].

Past cognition always believes that in Fenton or Fenton-like AOP system, NO oxidation induced by hydroxyl radical (HO•) is the most efficient reaction path [8], and hydrogen peroxide (H₂O₂) is often used

as the precursor due to its advantages of low cost and environmental friendly [9]. To boost the HO• yield and increase the H₂O₂ utilization, various Fe-based materials (e.g., Fe⁰, Fe₂O₃, Fe₃O₄, Co-Fe, Cu-Fe, Mn-Fe and FeOOH, etc) and different catalytic modes (e.g., heat, light, electricity and ultrasound, etc) have been developed and used [10–13]. However, their catalytic activity towards H₂O₂ is still not so good due to the inefficient circulation of Fe(II)/Fe(III) and the great loss of H₂O₂ during the radicals back-forth conversion [6]. On the other hand, in terms of the reactivity of various reactive oxygen species (ROS), more and more researchers have been aware of that the non-radical singlet oxygen (¹O₂) with longer lifetime (about 4 us), higher selectivity and stronger reactivity [14,15], appears superior ability than •OH (shorter lifetime, 10⁻³ us, and nonselective) in the degradation of electron-rich water organic pollutants and certain volatile organic compounds (VOCs), thus ¹O₂ has attracted increased attention in recent years. According to the quantum chemistry calculation, we also demonstrated that ¹O₂ could act as a bridge to boost the NO conversion process via lowering the energy barrier from NO to NO₃, but the formation of ¹O₂

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from the direct activation of H_2O_2 was still a challenge. To date, $^1\text{O}_2$ is mainly generated by the activation of peroxydisulfate (PMS) using heterogeneous catalysts, such as CoN_{2+2} , Cu-SA/MXene, Fe/O-doped g- C_3N_4 , et al. [16–18]. The asymmetric PMS ($\text{HO}-\text{O}-\text{SO}_3^-$) has three types of O atoms, which can provide different O atom coordination for catalysts, resulting in different trends of O-O and O-H breakage during PMS activation, thus can selectively split PMS to generate $^1\text{O}_2$ by modulating the coordination environment of the catalyst with O atoms [18,19]. In contrast, the symmetrical structure of H_2O_2 ($\text{HO}-\text{OH}$) with two identical O atoms cannot form differential O coordination with the catalytic site, so it is difficult to activate H_2O_2 generating multiple ROS, especially $^1\text{O}_2$ [19].

The latest researches clarified that high-valent oxides such as Co^{4+} and Mo^{6+} were capable of activating superoxide radicals ($\text{O}_2^{\bullet-}$) to generate $^1\text{O}_2$ [20,21]. It is lucky that ABO_3 -type perovskite iron oxides (LaFeO_3) contains high-valent iron state Fe(IV) and also can activate H_2O_2 into $\text{O}_2^{\bullet-}$ [22], thus LaFeO_3 with more Fe(IV) sites may be a good candidate for catalyzing H_2O_2 to directly generate $^1\text{O}_2$. However, the number of high-valent B-sites exposed by normal perovskite is limited, a modulation strategy is needed to further increase the number of high-valent B-sites exposed. Surface defects engineering can improve the electronic structure and surface chemical property of the normal perovskite materials, which can empower the perovskite catalyst with excellent ability of electron transfer and reactants adsorption [23,24]. For example, (i) A-site defect produced via doping or substitution methods, e.g. introducing Sr, Ca and Cu atoms into A-site to modulate its structure, can greatly improve its catalytic activity toward H_2O_2 and PMS to yield more ROS [25,26]; (ii) non-doping methods like non-stoichiometric strategy [27,28], urea modulation configuration and surface acid etching can boost the oxygen vacancy (OV) quantity [29, 30], improve the pore structure and increase the surface area, which can strengthen the mass transfer and reactants adsorption as well as possibly increasing the ROS yield. Hence, integrated utilization/modulation of these modification methods to develop an advanced Fe-based perovskite heterogeneous Fenton catalyst may yield a large number of $^1\text{O}_2$ from H_2O_2 activation and also achieve a better NO removal performance.

Herein, the present study prepared a novel LaFeO_3 heterogeneous Fenton catalyst via modulating its surface defects using non-stoichiometric and urea treatment methods, from which the abundant A-site defects, OVs and Fe(IV) active sites on the surface were formed simultaneously. In particular, urea-modulated LaFeO_3 could effectively

activate H_2O_2 to generate $^1\text{O}_2$, which was found to be superior to $\bullet\text{OH}$ and $\text{O}_2^{\bullet-}$ in NO removal, and this $\text{LaFeO}_3/\text{H}_2\text{O}_2$ system achieved the cost-effective removal of NO, with high gas hourly space velocity (GHSV) and low $\text{H}_2\text{O}_2/\text{NO}$ molar ratio. Based on the characterization and theoretical calculation results, the mechanisms of urea-modulated LaFeO_3 activating H_2O_2 to generate various ROS and the NO removal induced by different ROS were proposed.

2. Experimental Section

2.1. Synthesis of catalysts

All reagents used in this study are listed in Text S1. LaFeO_3 , La_xFeO_3 ($x = 0.6, 0.7, 0.8, 0.9$) and $x\text{U-LaFeO}_3$ ($x = 1, 2.5, 3.5, 5$) were synthesized via one-pot sol-gel method [24], and the fabrication scheme of these materials was shown in Fig. 1. (i) *Synthesis of LaFeO_3* : 2.60 g $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ and 2.43 g $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ were dissolved in 40 mL of deionized water at room temperature under stirring for 3 h. Subsequently, 2.78 g citric acid was added and stirred vigorously at 80°C until the sol was formed, then this sol was dried overnight at 110°C to obtain the spongy-like solid, which was ground and calcined in a muffle furnace at 700°C for 5 h. (ii) *Synthesis of La_xFeO_3* : the procedure was identical to the LaFeO_3 synthesis, except that the amount of $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ added was different. The obtained products were named as $\text{La}_{0.6}\text{FeO}_3$, $\text{La}_{0.7}\text{FeO}_3$, $\text{La}_{0.8}\text{FeO}_3$ and $\text{La}_{0.9}\text{FeO}_3$, respectively, with respect to the molar ratio of La/Fe of 0.6, 0.7, 0.8 and 0.9. (iii) *Synthesis of $x\text{U-LaFeO}_3$* : the procedure was the same as the LaFeO_3 synthesis, except that a certain amount of urea was added to the synthesis process. Specifically, when the molar ratio of urea and $\text{La}+\text{Fe}$ was 1, 2.5, 3.5 and 5, the obtained products were named as U-LaFeO_3 , 2.5 U-LaFeO_3 , 3.5 U-LaFeO_3 and 5 U-LaFeO_3 , respectively. The synthesis of 2.5 U-LaMnO_3 was the same as that of 2.5 U-LaFeO_3 , except that $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ was replaced to $\text{Mn}(\text{NO}_3)_2$ solution in the synthesis process.

2.2. Characterization methods

The actual compositions of sample was determined by Inductively Coupled Plasma Optical Emission Spectrometer (ICP-OES) technique (PE-7000DV, USA); the phase and crystal structure of samples were obtained by X-ray diffractometer (XRD, Bruker D8 advance); the surface chemical composition was analyzed by Fourier Transform Infrared

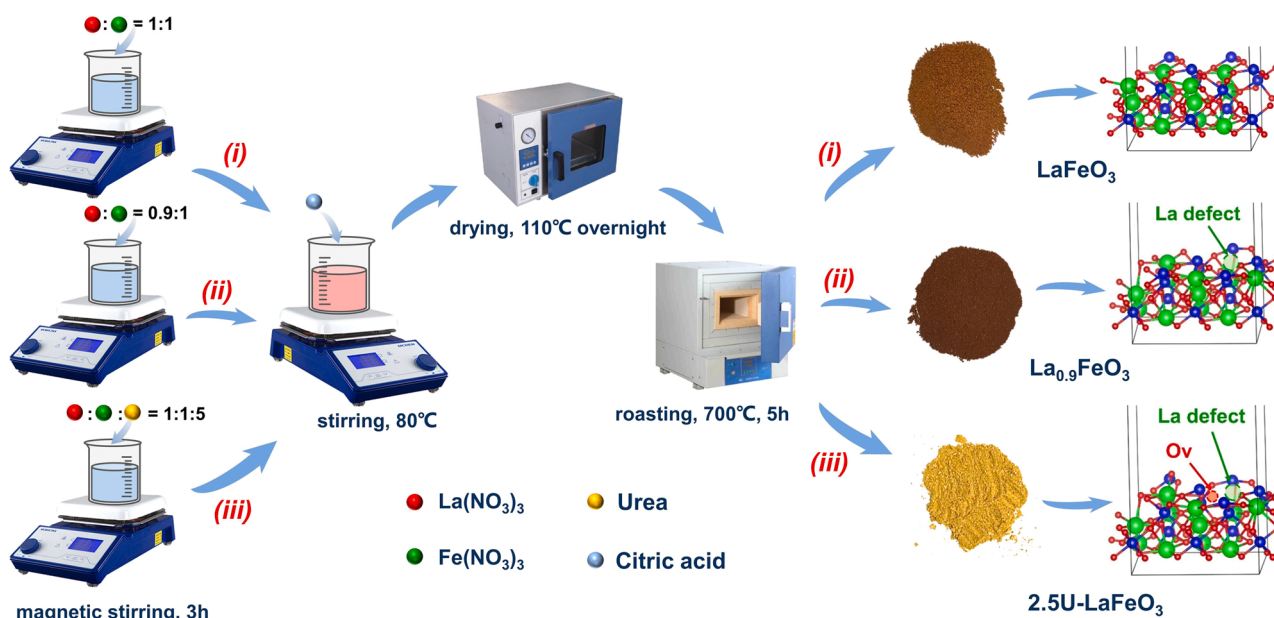


Fig. 1. Schematic illustration of the synthesis process of LaFeO_3 , $\text{La}_{0.9}\text{FeO}_3$ and 2.5U- LaFeO_3 catalysts.

Spectroscopy (FT-IR, Bio-Rad FTS-6000). The morphologies of materials were observed by scanning electron microscope (SEM, JSM-7500 F), high-resolution transmission electron microscopy (HRTEM, JEM-2100) and EDX elemental mapping. The nitrogen adsorption-desorption isotherms were applied to analyze the specific surface area, pore size and pore capacity of the catalysts; X-ray photoelectron spectroscopy (XPS, ESCALAB 250Xi) and energy spectroscopy (EDX) were used to analyze the active components on the catalyst surface. The reducibility and oxidizability of the samples were characterized by H_2 temperature programmed reduction (H_2 -TPR) and O_2 temperature programmed desorption (O_2 -TPD), respectively; the surface charge of samples were recorder by the Zeta potential analyzer. The yield of oxygen vacancy (Ov) and the radical species in the reaction system were identified by electron spin resonance spectrometer (EPR, Bruker EMX-E spectrometer). The ^{57}Fe Mössbauer spectra of compounds 1 and 2 were recorded on an SEE Co W304 Mössbauer spectrometer, using a $^{57}\text{Co}/\text{Rh}$ source in transmission geometry. The data were fitted by using the MossWinn 4.0 software.

2.3. Experimental procedure

The experimental flow is shown in Fig. S1, which consists of three parts: the simulated flue gas generation unit, the catalytic oxidation-absorption unit and the exhaust gas detection unit, all pipelines are made by Teflon. The simulated flue gas consists of N_2 , NO, SO_2 , CO_2 and O_2 with the total flow rate of 1 L/min, controlled by reducing valves and mass flow controllers. To generate the vaporized oxidant, the H_2O_2 solution was continuously pumped into a self-made evaporation reactor by a peristaltic pump at a rate of 256 $\mu\text{L}/\text{min}$ and vaporized by a thermally controlled electric heater. The vaporized oxidant was then carried by the simulated flue gas into a quartz tube (the diameter of 1 cm, the length of 400 cm) heated by a tube furnace, where the NO catalytic oxidation reaction occurred, and then the oxidation products were absorbed by 150 mL of 0.24 M Na_2SO_3 solution or H_2O . In addition, the catalyst dosage for each denitrification experiment was 0.1 g, while the gas hourly space velocity (GHSV) was $77,000\text{ h}^{-1}$. The flue gas concentration was recorded by a multifunctional flue gas analyzer, and the NO removal efficiency was calculated via Eq. 1, and the molar ratio of H_2O_2/NO was obtained via Eq. 2:

$$\eta = \frac{C_{in} - C_{out}}{C_{in}} \times 100\% \quad (1)$$

$$\delta = \frac{n_{H_2O_2}}{n_{NO}} = \frac{\frac{\omega \times \rho_{H_2O_2} \times V_{H_2O_2}}{34}}{\frac{C_{NO} \times Q}{30}} \quad (2)$$

Where η is the NO removal efficiency; C_{in} and C_{out} are the inlet and outlet concentrations of NO, mg/m^3 ; δ is the molar ratio of H_2O_2/NO ; ω is the mass fraction of H_2O_2 , wt%; $\rho_{H_2O_2}$ is the density of H_2O_2 ; $V_{H_2O_2}$ is the volume of H_2O_2 , uL/min ; C_{NO} is the NO concentration, mg/m^3 ; Q is the flue gas flow, m^3/min .

2.4. Density functional theory (DFT) calculation

DFT was performed using the Vienna ab initio Simulation Package (VASP). The interactions of core and nucleus with valence electrons are treated by the projective augmented wave (PAW) method, and the exchanges and correlations are described using the Perdew-Burke-Ernzerhof (PBE) functional. The (110) facet of LaFeO_3 was built with 2×1 supercell, and a vacuum layer of 15 Å was added to separated neighboring slabs to avoid possible interaction. Sampling of the Brillouin zone using a $2 \times 2 \times 1$ mesh of Monkhorst-Pack k-points for structural relaxation. The plane-wave cutoff energy was set at 400 eV. In the fully relaxed structure, the forces acting on all atoms were $< 0.02\text{ eV}/\text{\AA}$, and the electronic loops were self-consistent to an accuracy of 10^{-5} eV . The spin polarization of transition metal atoms was also considered. To

obtain the transition state structure, the climbing-image nudged elastic band (CI-NEB) method was adopted, and the vibration frequency analysis was performed using a finite displacement of $\pm 0.02\text{ \AA}$ to verify the minima and transition state structure. The configurations of $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 were constructed based on the orthorhombic LaFeO_3 system. One La atom was removed in the LaFeO_3 supercell to match the experimental composition $\text{La}_{0.9}\text{FeO}_3$, and one La and O atom were removal simultaneously to match 2.5 U- LaFeO_3 . The adsorption strength of gas molecules on the catalyst surface was calculated using Eq. 3:

$$E_{ads} = E_{adsorb} - E_{sur} - E_{gas} \quad (3)$$

where E_{adsorb} , E_{sur} and E_{gas} are the total energies of adsorption systems, catalyst surface and gases, respectively.

To describe the possible reaction pathways for $\text{HO}\bullet$, $\text{O}_2\bullet^-$, $\text{HO}_2\bullet$ and $^1\text{O}_2$ induced NO removal, DFT (MP2) calculations were performed using the Gaussian program package (G09W), and the reaction energy barriers for each step were calculated to predict the difficulty of each reaction from its energy perspective. The reliability was verified by frequency calculations of vibrational modes, and the performance of NO oxidation by $\text{HO}\bullet$, $\text{O}_2\bullet^-$, $\text{HO}_2\bullet$ and $^1\text{O}_2$ was predicted thermodynamically. Gaussian calculations were performed at the 6-311 G (d, p) basis group level.

3. Results and discussion

3.1. Catalysts characterizations

The elemental proportions of LaFeO_3 , $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 were analyzed by ICP-OES. In Fig. 2(a) and Table S1, the molar ratio of La to Fe is $0.96 (\text{LaFeO}_3) > 0.91 (\text{La}_{0.9}\text{FeO}_3) > 0.87 (2.5\text{ U-LaFeO}_3)$, confirming that urea modulation and non-stoichiometric synthesis could lead to the La-site defects. Owing to the similar size, NH_4^{+} (1.44 \AA) generated via urea pyrolysis can replace part of La^{3+} (1.36 \AA) in LaFeO_3 , and has a weak interaction with the surface FeO_6 octahedra, leading to the formation of N-H-O-Fe staggered conformation [31,32]. Besides, during urea pyrolysis process, N-H can also migrate out from the crystalline phase, resulting in the formations of La and O defects. In Fig. S2, the N 1s XPS spectra of LaFeO_3 , $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 and the EDX spectrum of 2.5 U- LaFeO_3 reveal the absence of N species on 2.5 U- LaFeO_3 surface, further confirming that urea can migrate out from the perovskite crystal phase at high temperature. The crystalline phases of the three catalysts were characterized by XRD. In Fig. 2(b), all of the three catalysts have the same and obvious characteristic peaks at 22.63° , 32.22° , 39.73° , 46.21° , 52.04° , 57.45° , 67.41° , 76.70° and 85.63° , corresponding to the diffraction planes of (100), (110), (111), (200), (210), (211), (220), (310) and (222), respectively, indicating the LaFeO_3 orthorhombic crystal phase (PDF# 75-0541). Their phase structures were also determined by XRD Rietveld refinement (Fig. S3), demonstrating their orthorhombic symmetry with a *Pnma* space group. Their FT-IR spectra all appear strong adsorption peaks at 553 cm^{-1} (Fig. S4), attributing to the Fe-O stretching vibration of the FeO_6 group [33]. Thus, the urea modulation and non-stoichiometric synthesis did not change the bulk phase structure of the catalysts.

The morphological and microstructural features of LaFeO_3 , $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 were imaged by SEM and HRTEM. In Fig. 2(c), the three samples all appear in the form of smooth wormlike rods, while 2.5 U- LaFeO_3 is more porous and well dispersed. In Fig. 2(d), LaFeO_3 has normal interface, while $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 appear defects, and the lattice fringe size of the primary (110) facet is decreased from 0.284 nm (LaFeO_3) to 0.283 nm ($\text{La}_{0.9}\text{FeO}_3$) and 0.281 nm (2.5 U- LaFeO_3), suggesting that modulation process smaller the lattice fringe spacing and caused the lattice distortion. The increase in the surface and edge defects due to urea modulation and non-stoichiometric synthesis will be favorable to increase the active sites for reactants adsorption [34,

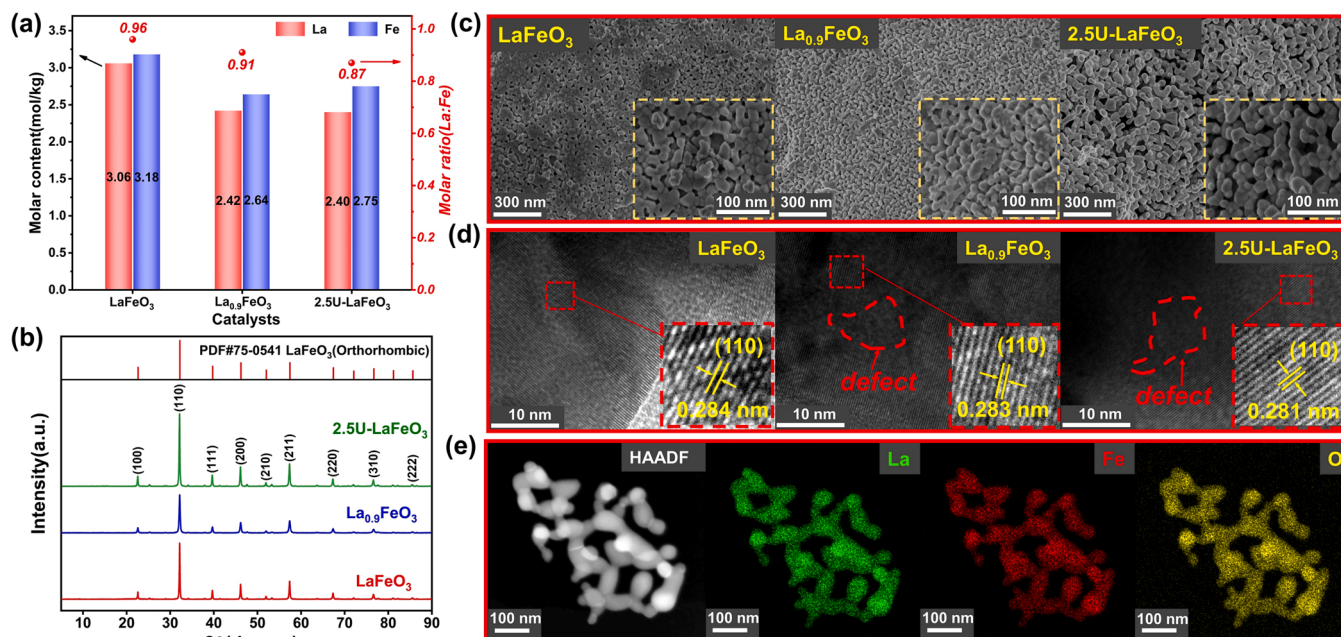


Fig. 2. (a) Molar content and the ratio of La to Fe in LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃; (b) XRD patterns of LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃; (c) SEM and (d) HRTEM images of LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃; (e) EDX element mapping images of 2.5 U-LaFeO₃.

35]. In Fig. 2(e), the EDX mappings confirms the uniform distribution of La, Fe, and O on the surface of 2.5 U-LaFeO₃. In Fig. 3(a), the nitrogen adsorption-desorption isotherms of LaFeO₃, La_{0.9}FeO₃, and 2.5 U-LaFeO₃ illuminate that all curves belong to the type IV hysteresis line (H3 type) according to the IUPAC [36], indicating that the three catalysts are mesoporous materials. The surface area in descending order is 29.278 m²/g (2.5 U-LaFeO₃) > 8.137 m²/g (La_{0.9}FeO₃)

> 7.634 m²/g (LaFeO₃), as consistent with the variation in the pore volume. However, the pore diameter has an opposite order: 13.158 nm (2.5 U-LaFeO₃) < 17.449 nm (La_{0.9}FeO₃) < 23.500 nm (LaFeO₃). Due to its largest specific surface area and best pore structure, 2.5 U-LaFeO₃ could expose the most active sites to boost the catalytic reaction by enabling better access to both reactants and peroxide [27].

The surface chemical compositions and elemental valence state of

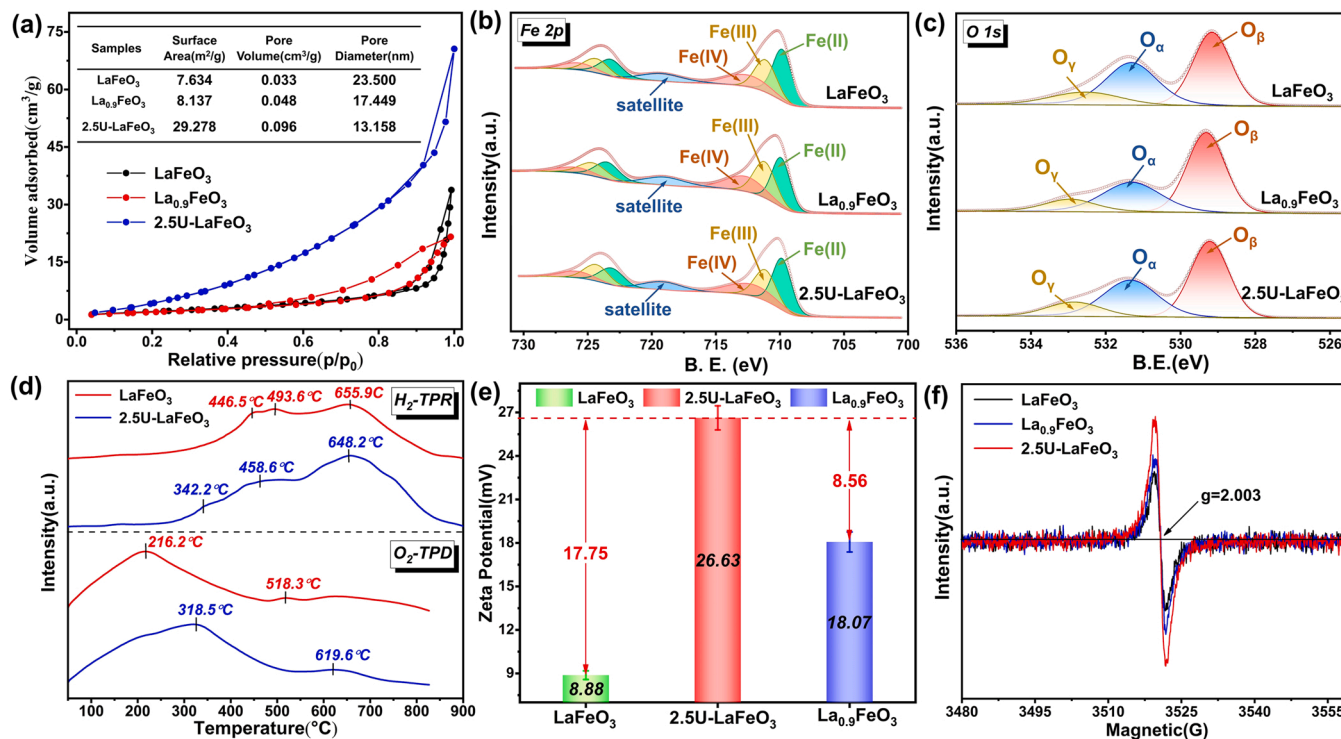


Fig. 3. (a) The nitrogen adsorption-desorption isotherms of LaFeO₃, La_{0.9}FeO₃, and 2.5 U-LaFeO₃, the inset table is the specific surface area and pore characteristic of these three samples; (b) Fe 2p and (c) O 1s XPS spectra of LaFeO₃, La_{0.9}FeO₃, and 2.5 U-LaFeO₃; (d) O₂-TPD and H₂-TPR curves of LaFeO₃ and 2.5 U-LaFeO₃; (e) Zeta potential and (f) EPR spectra of LaFeO₃, La_{0.9}FeO₃, and 2.5 U-LaFeO₃.

LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃ were further determined by XPS. In Fig. S5, the La 3d XPS spectra of the three catalysts all show four main peaks at 854.9, 851.8, 838.0 and 834.2 eV, corresponding to the La(III) 3d_{3/2}, La(II) 3d_{3/2}, La(III) 3d_{5/2} and La(II) 3d_{5/2} [31,37]. In Table S2, the La(II) contents of LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃ are 47.80%, 51.99% and 49.10%, respectively, which are 52.20%, 48.01% and 50.90% for La(III), indicating that non-stoichiometric synthesis and urea modulation would result in the conversion of partial La(III) to La(II). The Fe 2p XPS spectra in Fig. 3(b) can be resolved into six main peaks, in which Fe 2p_{3/2} at 709.8 eV and Fe 2p_{1/2} at 723.2 eV are assigned to Fe (II), Fe 2p_{3/2} at 711.1 eV and Fe 2p_{1/2} at 724.3 eV are attributed to Fe (III), and Fe 2p_{3/2} at 712.6 eV and Fe 2p_{1/2} at 725.8 eV are corresponding to Fe(IV). Besides, the peak located at 719.2 eV is a satellite peak [38,39]. In Table S2, the concentrations of Fe(II)/Fe(III)/Fe(IV) of LaFeO₃ are 45.11%, 32.02% and 22.87%, respectively, which are varied to 39.29%, 35.48% and 25.23% for La_{0.9}FeO₃, and to 41.01%, 33.46% and 25.53% for 2.5 U-LaFeO₃, suggesting that non-stoichiometric synthesis and urea modulation led to the conversion of Fe(II) to Fe (III)/Fe(IV) because of the formations of La and O defects. Such increase in the valence of the B-site cation will enhance the catalyst's oxidizability via facilitating the electron transfer between the reactants and the catalyst [39]. The O 1s XPS spectra in Fig. 3(c) can be divided into three peaks at 529.2, 531.3 and 532.8 eV, corresponding to the lattice oxygen (O_l), the surface chemisorbed oxygen (O_a), and the physically adsorbed oxygen such as water and other weakly bounded oxygen species (O_w), respectively [31,38]. In Table S2, the O_a content in descending order is 38.64% (LaFeO₃) > 34.16% (2.5 U-LaFeO₃) > 31.22% (La_{0.9}FeO₃), implying that both of non-stoichiometric synthesis and urea modulation would decrease the O_a content.

O₂-TPD is employed to investigate the distribution of oxygen species on the catalysts. In Fig. 3(d), two O₂ desorption peaks are clearly observed on LaFeO₃ and 2.5 U-LaFeO₃. The first peak at 216.2 °C for LaFeO₃ and at 318.5 °C for 2.5 U-LaFeO₃ is attributed to the desorption of surface active oxygen species [40–42], and such high temperature shift after urea modulation is due to the increase in oxygen vacancies (OVs) which stronger the bond with O₂ [27]. The second weak peak at 518.3 °C for LaFeO₃ and at 619.6 °C for 2.5 U-LaFeO₃ is assigned to the desorption of lattice oxygen in bulk phase [42], and the increase in desorption temperature after urea modulation is because the Fe-O bond becomes shorter owing to the La cation stripping [30]. The oxidizing capacity of LaFeO₃ and 2.5 U-LaFeO₃ were also studied by H₂-TPR in Fig. 3(d). Generally, La³⁺ is less susceptible to reduction below 1000 °C, so the reduction peaks observed in the TPR curves are attributed to the reduction of Fe species [40,43]. Three H₂ desorption peaks can be observed, in which the former two peaks below 550 °C are attributed to the reductions of Fe(IV) to Fe(III) and the surface Fe(III) to Fe(II), respectively, while the latter one peak above 550 °C belongs to the reductions of bulk Fe(III) to Fe(II) and Fe(II) to Fe(0) [43,44]. It can also be found that the urea treatment remarkably decreases the desorption temperatures from 446.5 to 342.2 °C and from 493.6 to 458.6 °C, respectively, indicating that the oxidizing capacity of Fe(IV) and the surface Fe(III) becomes stronger after urea treatment.

The surface charge of the three catalysts was determined by using Zeta potential method. In Fig. 3(e), the Zeta potential of 2.5 U-LaFeO₃ is 26.63 mV, which is far higher than those of La_{0.9}FeO₃ (18.07 mV) and pure LaFeO₃ (8.88 mV), indicating that the urea-modulated LaFeO₃ possessed the strongest adsorption capacity towards H₂O₂. Generally, the more positively charged surface of the oxide, the more anionic surface defects may appear, namely OV [27]. So we further used EPR analysis to investigate the OV quantity on the surface of LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃. In Fig. 3(f), the OV's peak intensity of 2.5 U-LaFeO₃ (19,852.46) is about 1.5 and 1.8 times as much as those of La_{0.9}FeO₃ (13,749.57) and LaFeO₃ (11,119.49), implying that urea modulation indeed facilitated the OVs' construction, and this result also well supported the O₂-TPD and Zeta potential analyses.

3.2. Heterogeneous Fenton denitrification performance

The heterogeneous Fenton denitrification performance of La₂O₃, Fe₃O₄, Fe₂O₃, LaFeO₃, La_{0.9}FeO₃, 2.5 U-LaFeO₃ and 2.5 U-LaMnO₃ were compared in Fig. 4(a). The NO removal efficiency is merely 37.09% when only using 3 wt% H₂O₂; after adding catalysts, the NO removal efficiency sharply increases to 50.49%, 60.01%, 61.16%, 65.64%, 69.83%, 80.53% and 54.56% with respect to the catalysts of La₂O₃, Fe₃O₄, Fe₂O₃, LaFeO₃, La_{0.9}FeO₃, 2.5 U-LaFeO₃ and 2.5 U-LaMnO₃, apparently 2.5 U-LaFeO₃ is the best. In Fig. 3(a) and S6, the surface area in descending order is 1.870 m²/g (La₂O₃) < 6.914 m²/g (Fe₂O₃) < 7.634 m²/g (LaFeO₃) < 8.057 m²/g (Fe₃O₄) < 8.137 m²/g (La_{0.9}FeO₃) < 29.278 m²/g (2.5 U-LaFeO₃) < 46.823 m²/g (2.5 U-LaMnO₃), which is not consistent with the denitrification performance, indicating that the increase in specific surface area is not the main reason for the improvement of catalytic activity. Fig. 4(b) illustrates the effect of the urea ratio on NO removal. The NO removal efficiency increases from 74.48% to 80.53% as the urea ratio increases from 1 to 2.5, and then decreases to 71.08% as the ratio further increases to 5. This phenomenon indicated that the excess urea was unfavorable for NO removal due to the pore blockage and the decrease in specific surface area, as demonstrated in Fig. S7. On the other hand, if without H₂O₂, the NO removal efficiency by using 2.5 U-LaFeO₃ was only 7.12%, indicating that 2.5 U-LaFeO₃ alone was also inefficiently in removing NO. The NO removal performance by using non-stoichiometric La_xFeO₃ (x = 0.6, 0.7, 0.8, 0.9, 1.0) catalysts is also shown in Fig. S8. The results showed that the La_{0.9}FeO₃ was the best (69.83%) but still far from that of 2.5 U-LaFeO₃ (80.53%), thereby the urea modulation method was better than the non-stoichiometric synthesis method in terms of improving the Fenton activity.

The effects of GHSV and the H₂O₂ concentration on NO removal were also studied in Figs. S9 and 4(c). When the GHSV decreases from 92,400 to 30,800 h⁻¹, the NO removal efficiency increases sharply from 45.61% to 82.89%; raising the H₂O₂ concentration from 1%wt to 5%wt (the H₂O₂/NO molar ratio increases from 4.7 to 24.0) can increase the NO removal efficiency from 82.89% to 94.74%. In Table S3, we can find that 2.5 U-LaFeO₃/H₂O₂ developed in this study is superior to the previous similar studies in NO removal, especially the lowest H₂O₂/NO molar ratio and the relatively high GHSV value. In the following parts, the GHSV and the H₂O₂ concentration were selected as 77,000 h⁻¹ and 5% wt, respectively. Fig. 4(d) illuminates the effect of the reaction temperature: a 'volcano map' curve between the NO removal efficiency and the temperature is observed, the best temperature is 120 °C for both H₂O₂ vaporization denitrification (37.07%) and 2.5 U-LaFeO₃ induced heterogeneous Fenton denitrification (89.12%). Fig. S10 clarifies the effect of pH on NO removal: acidic conditions promote NO removal, and neutral has basically no effect, but alkaline conditions slightly inhibit NO removal. The 2.5 U-LaFeO₃ heterogeneous Fenton denitrification system is adaptive to a wide pH range and is superior to the conventional Fenton system [45]. In Fig. 4(e), NO, O₂ and CO₂ exhibit the slight inhibitory effects but SO₂ plays a favorable role in NO removal, indicating that NO, O₂ and CO₂ would compete with H₂O₂ for the limited active sites, however SO₂ could enhance the NO removal via the redox reaction between SO₂ and NO₂ under moisture atmosphere [46]. Besides, it can be observed from Fig. S11 that the promoting effect of SO₂ can cover up the inhibiting effect of O₂, and the NO removal efficiency is enhanced when O₂ and SO₂ are added simultaneously. After withdrawing O₂ and SO₂, the NO removal efficiency gradually recover to the initial level, indicating the stability of 2.5 U-LaFeO₃ denitrification performance. In Fig. 4(f), the reusability of 2.5 U-LaFeO₃ was evaluated, and the NO removal efficiency decreases only by 7% after fifth cycle. Moreover, the XRD and SEM patterns of the spent 2.5 U-LaFeO₃ shown in Figs. S12-S13 appear no significant variations in the crystalline phase and morphology, implying that 2.5 U-LaFeO₃ had excellent stability and reusability.

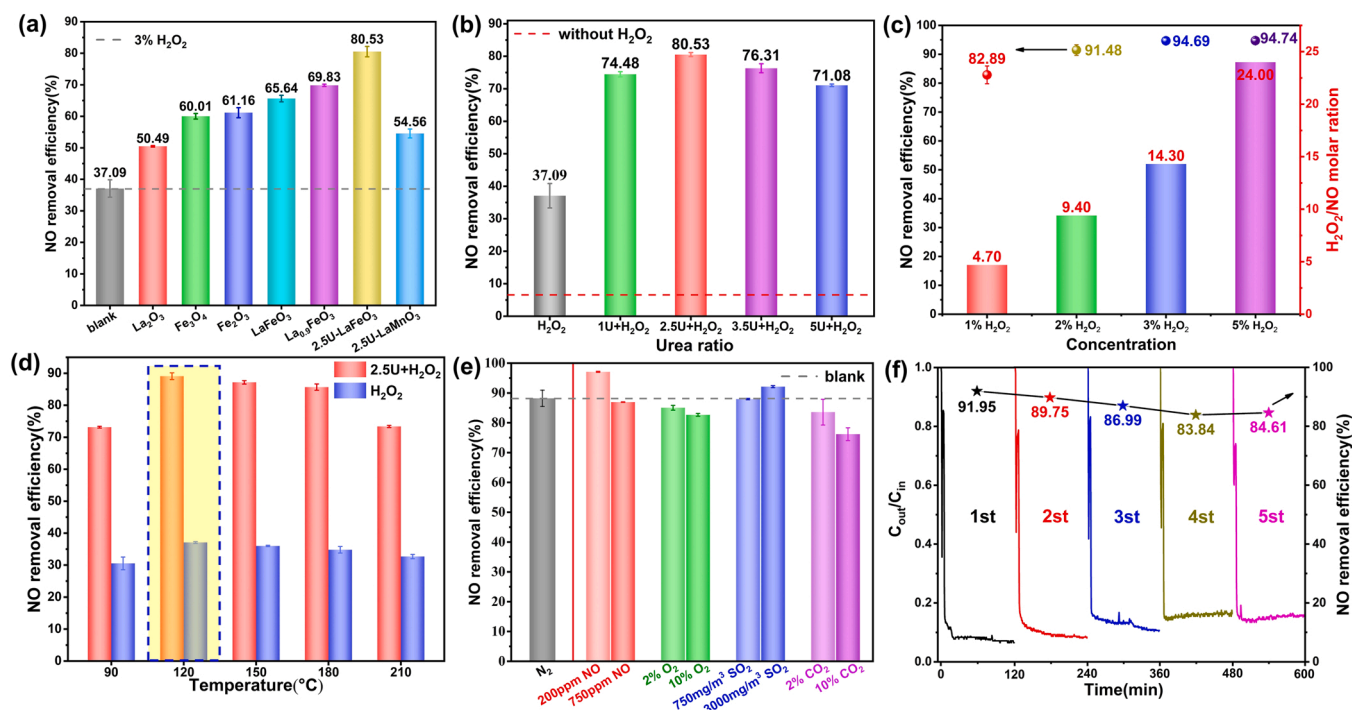


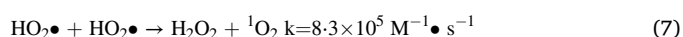
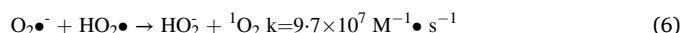
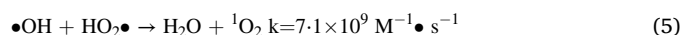
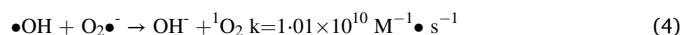
Fig. 4. (a) The performance of different catalysts for NO removal; (b) the influence of urea ratio on NO removal efficiency; (c) the influence of H₂O₂ concentration on NO removal efficiency and H₂O₂/NO molar ratio; (d) influences of temperature; (e) flue gas components (NO, O₂, SO₂ and CO₂) on the NO removal efficiency; (f) the reusability of 2.5 U-LaFeO₃ catalyst for NO removal process. Reaction conditions: NO concentration, 350 ppm; catalyst mass, 0.1 g; balance gas, N₂; gas flow, GHSV = 77,000 h⁻¹, temperature, 120 °C.

3.3. ROS determination and generation mechanisms

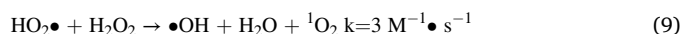
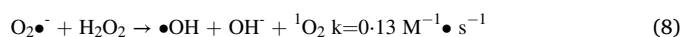
EPR tests were firstly performed to determine the ROS types in 2.5 U-LaFeO₃/H₂O₂. The fingerprint peaks of DMPO-OH (1:2:2:1), DMPO-O₂^{•-} (sextet line signals) and 2,2,6,6-tetramethyl-4-piperidinol-N-oxyl (TEMPO, triple line signals) adducts appear in Fig. 5(a), confirming the formations of •OH, O₂^{•-} and ¹O₂ [47], and the peak intensities of ¹O₂ and O₂^{•-} are higher than those of •OH, suggesting that ¹O₂ and O₂^{•-} are the major ROS. In Fig. S14, the peaks intensity gradually enlarges as the reaction time increases from 1 min to 10 min, implying their longer presence and continual generation with the reaction time. To evaluate the contributions of •OH, O₂^{•-} and ¹O₂ to the NO removal, radical quenching tests were further carried out by using tert-butanol (TBA), p-benzoquinone (BQ) and furfuryl alcohol (FFA) as the scavengers, respectively [48]. In Fig. 5(b), adding TBA, BQ and FFA all reduce the NO removal efficiency, and the inhibitory rate in descending order is FFA (53.66%) > BQ (19.53%) > TBA (10.22%), indicating that the contribution order of ROS to NO removal is ¹O₂ > O₂^{•-} > •OH. To confirm whether TBA, BQ and FFA consume H₂O₂, the H₂O₂ content in H₂O₂, H₂O₂ + FFA and H₂O₂ + BQ systems was determined using the KMnO₄ titration method in Fig. S15 (Text S2), and the results showed that FFA or BQ did not consume H₂O₂ and only acted as the radical quencher. Besides, ozone (O₃) concentration in this system was detected (Fig. S16): the steady O₃ concentration was only 1.81 ppm, so its contribution to NO removal (350 ppm) was negligible. The EPR spectra of ¹O₂ under O₂ atmosphere is also provided in Fig. S17: only a weak peak signal appears at the beginning, and the existence time was too short to maintain NO removal. Given the facts that ¹O₂ dominated the NO removal process and H₂O₂ was the sole ROS precursor in this system (N₂ atmosphere), three possible reaction pathways of H₂O₂ deriving into ¹O₂ were summarized in Fig. S18: (i) the radical self-quenching reactions including the recombination of O₂^{•-} and HO₂[•], and the reactions between O₂^{•-}/HO₂[•] and •OH (Eqs. 4–7) [49,50]; (ii) the Haber-Weiss reaction between O₂^{•-}/HO₂[•] and H₂O₂ (Eqs. 8–9) [51,52]; (iii) the oxidation reaction between high-valent metal cations and O₂^{•-} (Eqs.

10–11) [20,21].

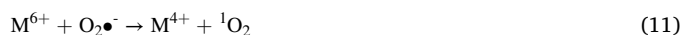
Path i:



Path ii:



Path iii:



In Paths (i) and (ii), the rate constants involving •OH (Eqs. 4–5) for ¹O₂ generation are far higher than others (Eqs. 6–9), so we firstly determined if •OH contributed the most to the ¹O₂ yield. In Fig. 5(c), when 90 mM TBA is added in the 2.5 U-LaFeO₃/H₂O₂, the EPR signal intensity of TEMPO is unchanged, indicating that the reactions between O₂^{•-}/HO₂[•] and •OH are helpless for ¹O₂ generation. Besides, in Path (ii) the Haber-Weiss reaction is highly dependent on the high concentration of H₂O₂ [47,50], so we studied the contribution rate of ¹O₂ to the NO removal under different H₂O₂ concentrations. In Fig. 5(d), as the H₂O₂ concentration increases by 2 times, the ¹O₂ contribution rate to the NO removal decreases by 9.1% instead, indicating that the concentration of H₂O₂ was not the primary factor dominating the ¹O₂ yield.

Learned from the above analyses, Path (iii) is the most probability. To prove this, we added BQ to quench O₂^{•-} to suppress its reaction with Fe(III) and Fe(IV). In Fig. 5(c), after adding 90 mM BQ, the signal intensity of TEMPO dramatically decreases, confirming the involvement of

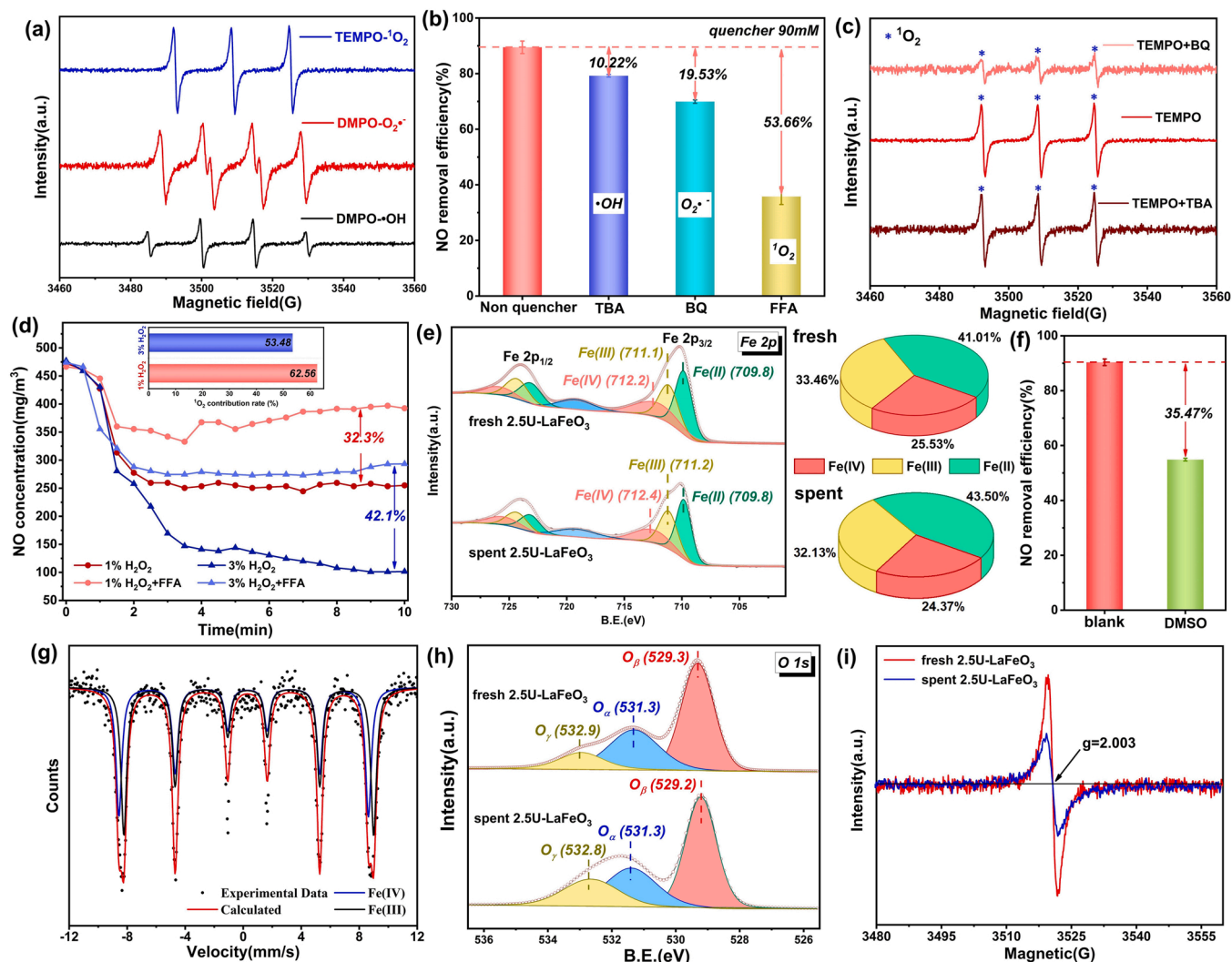


Fig. 5. (a) EPR spectra of the activated H_2O_2 system using DMPO and TEMP spin-trapping; (b) The radical scavenging experiments during NO removal; (c) EPR spectra of $\cdot\text{O}_2$ in the presence of BQ and TBA; (d) quenching experiments with FFA as the scavenger under 1% and 3% H_2O_2 concentrations; the XPS spectra of fresh and spent 2.5 U-LaFeO₃; (e) Fe 2p; and (h) O 1s; (f) DMSO quenching experiment during NO removal; (g) Mössbauer spectrum of 2.5 U-LaFeO₃; (i) EPR profiles of fresh and spent 2.5 U-LaFeO₃.

$\text{O}_2^{\cdot-}$ in $\cdot\text{O}_2$ generation. Moreover, in Fig. 5(e) the Fe 2p XPS analyses of the fresh and spent 2.5 U-LaFeO₃ also illuminate that after reaction the proportions of Fe(IV) and Fe(III) decrease from 25.53% to 24.37% and from 33.46% to 32.13%, respectively, while that of Fe(II) increases from 41.01% to 43.50%. To solidly verify the involvement of Fe(IV)/Fe(III) in $\cdot\text{O}_2$ generation, the Mössbauer spectroscopy analysis and DMSO quenching experiment were further conducted. In Mössbauer spectroscopy, the isomer shifts (IS) can describe the charge density of the electron cloud around the charge and characterize the electrostatic interactions, so the valence state of material can be obtained according to IS [53]. DMSO, as a reductant, can reduce Fe(IV) to Fe(II) via a 2-electron transfer step [54,55], thereby reducing the content of Fe(IV) in material. In Fig. 5(g) and Table S4, it can be found from the Mössbauer spectrum of 2.5 U-LaFeO₃ that two isomer shifts appear, i.e. 0.34 and 0.16, representing the Fe(III) and Fe(IV) species, respectively [56,57]. In Fig. 5(f), after adding 0.36 M DMSO, the NO removal efficiency decreases by 35.47%, confirming the existence and the function of Fe(IV) in the heterogeneous Fenton denitrification reaction. Hence, the above analyses manifested that $\text{O}_2^{\cdot-} + \text{Fe(IV)/Fe(III)}$ is the main generation path of $\cdot\text{O}_2$.

To reveal the roles of each component of 2.5 U-LaFeO₃ in heterogeneous Fenton reaction, the elemental valence evolution of La and O in

the fresh and spent 2.5 U-LaFeO₃ catalysts were illuminated by XPS. In Fig. S19 and Table S2, the proportions of La(II) and La(III) are unchanged before and after the reaction, indicating that La was not involved in reaction [27,33]. But in Fig. 5(h) and Table S2, the proportion of O_α decreases from 34.16% to 28.49%, while that of O_β increases from 51.74% to 55.53%, indicating that the surface chemisorbed oxygen was consumed, whereas OV converted into the lattice oxygen by grabbing an O atom. To confirm this, we used EPR method to determine the OV's quantity in the fresh and spent 2.5 U-LaFeO₃. In Fig. 5(i), after reaction the OV's quantity decreases by a half (from 19852.46 to 9319.71), thus OV was definitely involved in the heterogeneous Fenton reaction and might serve as one of the adsorption sites for O-containing reactants [31].

3.4. Theoretical calculation and denitrification mechanisms

DFT calculations were used to study the heterogeneous Fenton mechanism, and the surface model of the (110) facet of LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃ was built. Firstly, two thermodynamically stable adsorption configurations of H_2O_2 on three catalysts were constructed in Fig. 6(a) and (b). In configuration (a), H_2O_2 can be decomposed into two $\cdot\text{OH}$ on a Fe atom, and the adsorption energies (E_{ads}) are

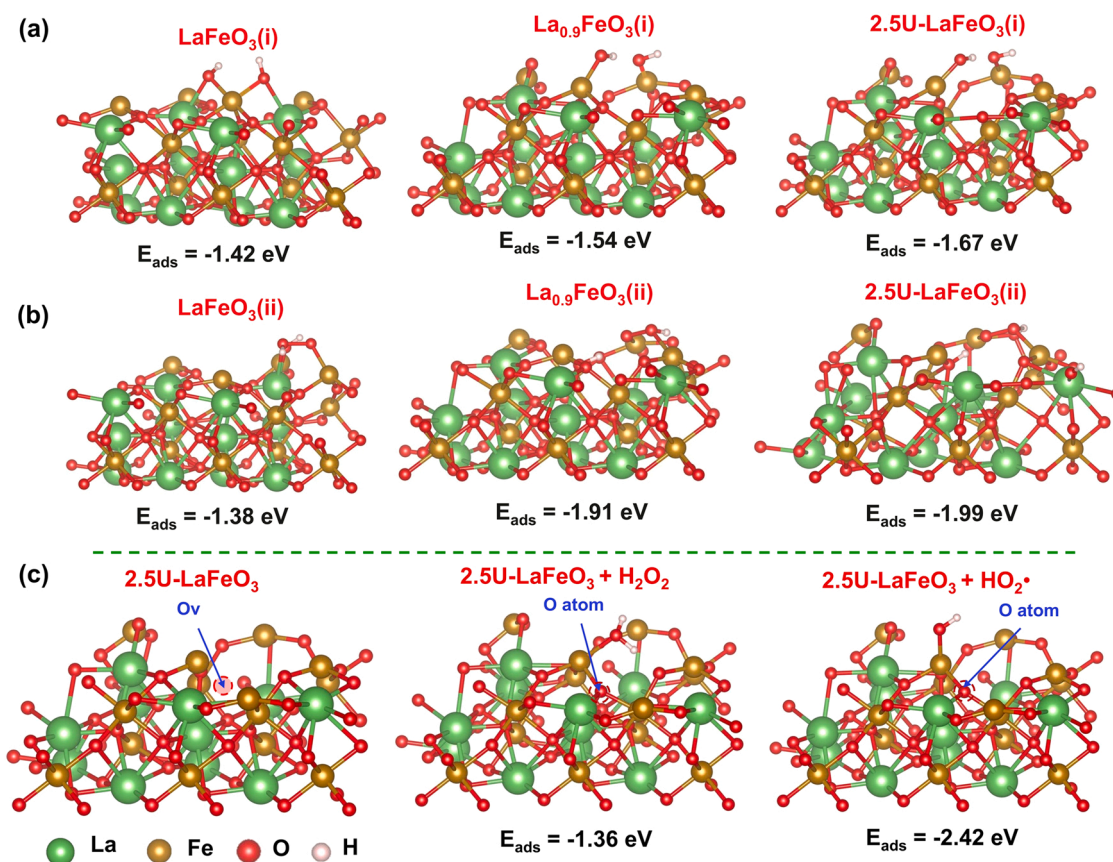


Fig. 6. (a, b) The configurations of H_2O_2 adsorption on LaFeO_3 (110), $\text{La}_{0.9}\text{FeO}_3$ (110) and 2.5 U- LaFeO_3 (110) surface; (c) the configurations of H_2O_2 and HO_2^\bullet adsorption on OV site of 2.5 U- LaFeO_3 .

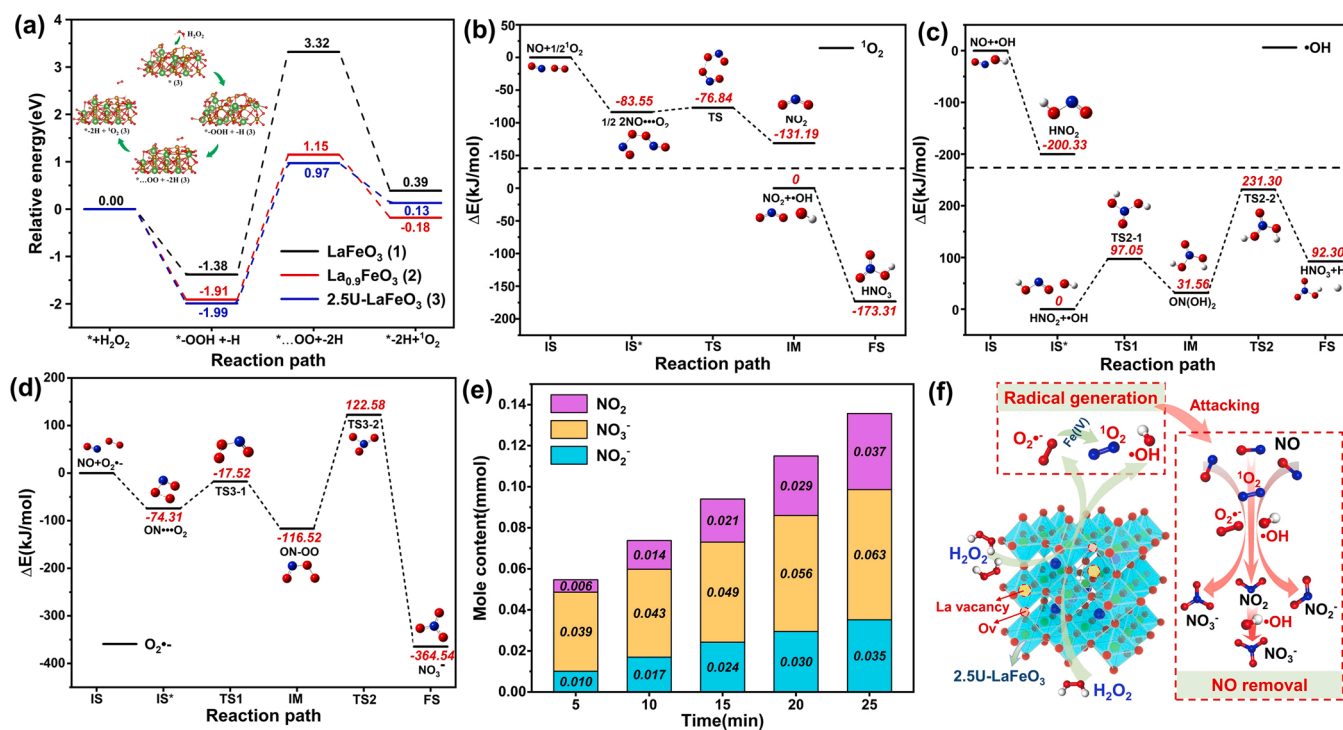


Fig. 7. (a) The energy variation along reaction paths over LaFeO_3 , $\text{La}_{0.9}\text{FeO}_3$ and 2.5 U- LaFeO_3 activating H_2O_2 ; theoretical calculation on (b) $^1\text{O}_2$, (c) $^\bullet\text{OH}$ and (d) $\text{O}_2^{\bullet-}$ initiated NO removal reactions; (e) the distribution and variation of N species in the tail gas and absorption liquid; (f) mechanism schematic of NO removal by 2.5 U- $\text{LaFeO}_3/\text{H}_2\text{O}_2$.

– 1.42, – 1.54 and – 1.67 eV for LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃, respectively. In configuration (b), H₂O₂ is decomposed into a HO₂[•] on a Fe atom and a -H on the bridge O atom of FeO₆ octahedron, the corresponding E_{ads} are – 1.38, – 1.91 and – 1.99 eV. The results indicated that the two reactions could proceed spontaneously, but the configuration (b) was more thermodynamically favorable. Moreover, the lowest E_{ads} of H₂O₂ on 2.5 U-LaFeO₃ suggested that urea-modulated LaFeO₃ was superior to LaFeO₃ and La_{0.9}FeO₃ in activating H₂O₂, which was mainly due to 2.5 U-LaFeO₃ had more OV sites, as proved by the DFT calculation and EPR analysis. To demonstrate the promotion of OV, the adsorption configurations of H₂O₂ and HO₂[•] on OV of 2.5 U-LaFeO₃ were constructed in Fig. 6(c). The results suggested that OV could trap an O atom from H₂O₂ or HO₂[•], which then decomposed into H₂O and •OH (on Fe atom), respectively, and the corresponding E_{ads} are – 1.36 and – 2.42 eV, so OV was easily to adsorb HO₂[•] instead of H₂O₂. Therefore, the •OH generation path could be concluded as following two: (i) Fe site could directly split H₂O₂ into two •OH; (ii) OV site decomposed the intermediate HO₂[•] into •OH.

To depict the ¹O₂ generation path, the transition state (TS) theory was used to calculate the energy variations along the reaction paths over LaFeO₃, La_{0.9}FeO₃ and 2.5 U-LaFeO₃, and the relevant energy and structural variations are presented in Fig. 7(a) and S20, respectively. With the configuration (b) in Fig. 6 as the adsorption model, H₂O₂ will be firstly adsorbed on the catalyst's slab (*) and decomposed into * -OOH and -H; afterwards the * -OOH will convert into the transition state * ...OO; finally ¹O₂ will be formed via electron transfer with Fe (IV)/Fe(III). Additionally, the order of the energy barrier from * -OOH to * ...OO is 4.70 eV (LaFeO₃) > 3.06 eV (La_{0.9}FeO₃) > 2.96 eV (2.5 U-LaFeO₃), indicating that both urea modulation and non-stoichiometric synthesis methods could improve the catalytic activity but urea modulation was better. Hence, the urea modulation method can not only enhance the adsorption capacity toward H₂O₂, but also reduce the reaction energy barrier for ¹O₂ generation.

Then the mechanism of NO removal induced by •OH, O₂^{•-} and ¹O₂ were depicted by using Gaussian 09 software. In Fig. 7(b), ¹O₂ can react with two NO to form a complex ON•••O-O•••NO, and then the O-O bond will be broken after undergoing a TS with the ΔE of only 6.71 kJ/mol, finally two NO₂ are formed. Subsequently, the formed NO₂ can spontaneously react with •OH to produce a HNO₃. In Fig. 7(c), •OH can spontaneously react with NO to form a HNO₂, then the formed HNO₂ continually reacts with a •OH to produce a HNO₃, but the ΔE values for TS2-1 (from HO-ON•••OH to ON(OH)₂) and TS2-2 (from ON(OH)₂ to HNO₃) are as high as 97.05 kJ/mol and 199.74 kJ/mol, respectively. In Fig. 7(d), O₂^{•-} can spontaneously react with NO to form a complex ON•••O₂, which then evolves into the intermediate ON-OO via TS3-1 (ΔE = 56.11 kJ/mol). Finally, undergoing TS3-2 (ΔE = 239.10 kJ/mol), the N-O bond in ON-OO is rotated, the O-O bond is elongated and the terminal O atom approaches N to form N-O, while the O-O bond breaks, NO₃ is formed eventually. In summary, ¹O₂ was responsible to the formation of NO₂, while •OH and O₂^{•-} mainly contributed to the formations of NO₂ and NO₃; the reactivity of the three ROS towards NO is ¹O₂ > •OH > O₂^{•-} according to the ΔE values; the main generation path for NO₃ could be NO₂ + •OH due to its lowest ΔE value; •OH played two major roles in the NO removal process: (i) direct oxidation of NO into NO₂; (ii) secondary oxidation of NO₂ into NO₃.

To identify the distribution and variation of N species in the system, the contents of NO₂, NO₂ and NO₃ in the tail gas and the absorption liquid were detected. In Fig. 7(e) and S21, as the reaction proceeds from 5 to 15 and 25 min, the proportion of NO₂ increases from 10.98% to 22.33% and 27.28%, while that of NO₃ decreases from 70.53% to 51.87% and 46.79%, and that of NO₂ slightly increases from 18.50% to 25.80% and 25.93%. The results implied that as the reaction proceeded, the quantity of •OH was insufficient to eliminate all NO₂, and •OH was inclined to directly react with NO to form NO₂ instead of with NO₂ to form NO₃, which was mainly due to their difference in ΔE values (–200.33 eV vs –173.31 eV). But it was worth noting that although the

proportion of NO₃ decreased gradually with the reaction, it was still the main N-product. In Fig. S22, if the absorption liquid was added with Na₂SO₃, the main N product turned from NO₃ to NO₂, and only a little NO₂ was emitted, which was resulted from the redox reaction between NO₂ and SO₃²⁻ [58]. The overall mechanisms of NO removal by 2.5 U-LaFeO₃/H₂O₂ are depicted in Fig. 7(f): (i) *Radical generation*: the 2.5 U-LaFeO₃ catalyst firstly adsorbs and decomposes H₂O₂ into •OH and HO₂[•]/O₂^{•-}, then OV catalyzes HO₂[•] to generate HO•, and Fe(IV)/Fe(III) catalyze O₂^{•-} to produce ¹O₂. (ii) *NO removal*: the generated •OH, O₂^{•-} and ¹O₂ selectively oxidize NO into NO₂, NO₃ and NO₂, in which the reactions of NO + ¹O₂, NO₂ + •OH and NO + •OH are the main pathways for the NO removal; O₂^{•-} is mainly acted as the precursor of ¹O₂ instead of an oxidant directly oxidizing NO into NO₃.

4. Conclusions

This study fabricates a urea-modulated perovskite catalyst 2.5 U-LaFeO₃, which can generate abundant ¹O₂ in the heterogeneous Fenton system, different from the conventional •OH-dominated Fenton reaction. A series of characterization methods confirmed that 2.5 U-LaFeO₃ had abundant La defects, OVs and Fe(IV) active sites, and the urea modulation also improved the pore structure of perovskite and increased the specific surface area, thus enhancing the absorption, splitting and utilization of H₂O₂. The LaFeO₃/H₂O₂ system could achieve cost-effective removal of NO (82.9%) at high GHSV (30,800 h⁻¹) and low H₂O₂/NO molar ratio (4.7), along with good environmental adaptability and reusability. ¹O₂, O₂^{•-} and •OH were the main radicals generated in this reaction system, among which ¹O₂ was superior to other radicals in NO removal. Combined the characterization and theoretical calculations, the ¹O₂ generation route in the 2.5 U-LaFeO₃/H₂O₂ system and the NO removal mechanisms induced by ¹O₂, O₂^{•-} and •OH were systematically depicted. Urea-modulated LaFeO₃ perovskite material is a superior, cost-efficient and simple-synthesis catalyst, which can provide a feasible and promising strategy for the development of heterogeneous Fenton denitrification technology.

CRediT authorship contribution statement

Zhen Qian: Data curation, Validation, Formal analysis, Writing – original draft. **Mengchao Luo**: Data curation, Visualization. **Xiaohe Feng**: Data curation. **Xiaojie Yang**: Data curation. **Yongxue Guo**: Data curation. **Lijuan Yang**: Supervision, Conceptualization. **Bo Yuan**: Supervision, Investigation. **Yi Zhao**: Resources, Supervision. **Runlong Hao**: Project administration, Funding acquisition, Writing – review & editing.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data Availability

Data will be made available on request.

Acknowledgments

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Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at doi:10.1016/j.apcatb.2023.123042.

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